

# Formation, dynamics and stability of coreless vortex dipoles in phase-separated binary condensates

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We study the motion of the Gaussian obstacle potential created by blue detuned laser beam through a phase-separated binary condensate in pancake-shaped traps. For the velocity of the obstacle above a critical velocity, we observe the generation of vortex dipoles in the outer component which can penetrate the inner component. This is equivalent to finite, although small, transport of outer component across the inner component. In the inner component, the same method can lead to the formation of coreless vortex dipoles.

## I. INTRODUCTION

Generation of vortex dipoles in dilute Bose-Einstein condensates (BECs) when a superfluid moves past an obstacle with a velocity greater than a critical velocity (speed of sound locally) has been established by various numerical studies [1]-[5]. It has been established, both theoretically and numerically, that even the flow of the BEC below bulk sound speed can result in the flow velocity greater than the local sound speed at the equator of the obstacle. It implies that the critical velocity for the creation of vortex-antivortex pairs is lower than the bulk sound speed. Above this critical speed vortex-antivortex pairs are created periodically, resulting in an oscillatory drag force. This is due to the phase difference between the main flow and stationary wake behind the obstacle. Whenever this phase difference grows to  $2\pi$  a vortex-antivortex pair is created. Recently, Neely et al. [6] observed the generation of vortex dipoles in a pancake-shaped  $^{87}\text{Rb}$  condensate, when the condensate was moved past a Gaussian obstacle, created by blue-detuned laser beam, above critical velocity. Real time dynamics of single vortex line and vortex dipoles has also been studied experimentally [7]. The flow of the miscible binary and spinor condensates across a Gaussian obstacle potential has also been investigated theoretically in Refs.[8-10]. Vortex dipoles or vortex rings are also produced as one of the decay products of dark solitons (a notch or density depression in the condensate with a phase slip of  $\pi$  across it), due to the onset of a transverse instability in 2D and 3D geometries, namely snake instability. The decay of dark soliton into vortex rings has already been observed experimentally [11, 12]. In this context, it should be noted that motion of the obstacle across a 1D BEC generates grey solitons [13-15]. The snake instability is also responsible for the decay of ring soliton into a necklace of vortex dipoles [16].

In the present work, we study the flow of phase-separated binary condensates across a Gaussian obstacle numerically. We consider two experimentally realizable binary condensates: the first of these has  $^{85}\text{Rb}$  and  $^{87}\text{Rb}$  and the second has the two hyperfine states of  $^{87}\text{Rb}$  as the two constituent species. In both these condensates, one

of the scattering length can be tuned by using magnetic Feshbach resonances [17, 18]. This allows us to choose the tunable scattering lengths values suitable for generation of coreless vortex dipoles. We observe the generation of vortex dipoles for the flow velocity greater than the critical velocity. In our simulations while moving the obstacle, its strength is continuously decreased. We consider two cases: (a) the obstacle laser potential, initially in the outer component, is moved towards the center, and (b) the obstacle laser potential, initially in the inner component, moves towards the interface of the binary condensate. With the successful realization of vortex dipoles in single component condensates using obstacle potential [6], the present studies give more than enough reasons to extend these experimental studies to binary condensates.

## II. BINARY CONDENSATES AND VORTEX DIPOLES

### A. Meanfield description of binary condensates

The dynamics of binary condensate at  $T = 0\text{K}$  can be very well described by a set of coupled GP equations

$$\left[ \frac{-\hbar^2}{2m} \nabla^2 + V_i(\mathbf{r}, t) + \sum_{j=1}^2 U_{ij} |\Psi_j(\mathbf{r}, t)|^2 - i\hbar \frac{\partial}{\partial t} \right] \Psi_i(\mathbf{r}, t) = 0 \quad (1)$$

in mean field approximation, where  $i = 1, 2$  is the species index. Here  $U_{ii} = 4\pi\hbar^2 a_{ii}/m_i$ , where  $m_i$  is the mass and  $a_{ii}$  is the  $s$ -wave scattering length, is the intra-species interaction,  $U_{ij} = 2\pi\hbar^2 a_{ij}/m_{ij}$ , where  $m_{ij} = m_i m_j / (m_i + m_j)$  is the reduced mass and  $a_{ij}$  is the inter-species scattering length, is the inter-species interaction, and  $V_i(\mathbf{r})$  is the trapping potential experienced by  $i$ th species. In the present work, we consider binary condensate consisting either of  $^{85}\text{Rb}$  and  $^{87}\text{Rb}$  for which  $m_1 \approx m_2$ . Furthermore, we also consider identical trapping potential for both the species, the total potential is then  $i$ th species

$$V(\mathbf{r}, t) = \frac{m_1 \omega^2}{2} (x^2 + \alpha^2 y^2 + \beta^2 z^2) + V_{\text{obs}}(x, y, t), \quad (2)$$

where  $V_{\text{obs}}(x, y, t) = V_0(t) \exp\{-2([x - x_0(t)]^2 + y^2)/w_0^2\}$  is the potential created by blue detuned laser beam, and  $\alpha$  and  $\beta$  are anisotropy parameters. To rewrite the coupled GP equations in scaled units, define the oscillator length of the trapping potential

$$a_{\text{osc}} = \sqrt{\frac{\hbar}{m\omega}}, \quad (3)$$

and consider  $\hbar\omega$  as the unit of energy. We then divide the Eq.(1) by  $\hbar\omega$  and apply the transformations

$$\tilde{\mathbf{r}} = \frac{\mathbf{r}}{a_{\text{osc}}}, \quad \tilde{t} = t\omega, \quad \text{and} \quad \phi_i(\tilde{\mathbf{r}}, \tilde{t}) = \sqrt{\frac{a_{\text{osc}}^3}{N_i}} \Psi_i(\mathbf{r}, t). \quad (4)$$

The transformed coupled GP equation in scaled units is

$$\left[ -\frac{\tilde{\nabla}^2}{2} + V_i(\tilde{\mathbf{r}}, \tilde{t}) + \sum_{j=1}^2 \tilde{U}_{ij} |\phi_j(\tilde{\mathbf{r}}, \tilde{t})|^2 - i \frac{\partial}{\partial \tilde{t}} \right] \phi_i(\tilde{\mathbf{r}}, \tilde{t}) = 0, \quad (5)$$

where  $\tilde{U}_{ii} = 4\pi a_{ii} N_i / a_{\text{osc}}$ ,  $\tilde{U}_{ij} = 4\pi a_{ij} N_j / a_{\text{osc}}$ , and  $\tilde{\nabla}^2 = a_{\text{osc}}^2 \nabla^2$ . From here on, we will represent the scaled quantities without tilde unless stated otherwise.

In pancake-shaped (highly oblate) traps, trapping frequency along axial direction is much greater than the radial directions, i.e.,  $\beta \gg \alpha \sim 1$ ; in which case Eq.(5) can be reduced to two dimensional form by substituting  $\phi(\mathbf{r}, t) = \psi(x, y, t) \xi(z) \exp(-i\beta t/2)$  [19]. Here  $\xi = (\beta/(2\pi))^{1/4} \exp(-\beta z^2/4)$ , the ground state wave function in axial direction. The reduced two dimensional form of coupled GP equation in pan-cake shaped traps is

$$\left[ -\frac{1}{2} \left( \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} \right) + \frac{x^2 + \alpha_i^2 y^2}{2} + U(x, y, t) + \sum_{j=1}^2 u_{ij} |\psi_j(\mathbf{r}, t)|^2 - i \frac{\partial}{\partial t} \right] \psi_i(\mathbf{r}, t) = 0, \quad (6)$$

where  $u_{ii} = 2a_{ii} N_i \sqrt{2\pi\beta_i} / a_{\text{osc}}$  and  $u_{ij} = 2a_{ij} N_j \sqrt{2\pi\beta_i} / a_{\text{osc}}$ . In the present work, we consider  $u_{12} > \sqrt{u_{11}u_{22}}$  so that the ground state of the binary condensate is phase-separated. The ground states of the binary condensates in the phase separated domain have been studied in Refs.[20]-[27]. In pancake-shaped traps the binary condensates has cylindrical interface separating the two components [26].

### B. Vortex dipole trajectory in a single component condensate

The total velocity field experienced by each vortex in vortex dipole is the vector sum of two component fields. One of these fields is the velocity field generated on each vortex due to inhomogeneous nature of the condensate in the trapping potential. This inhomogeneity generated velocity field is responsible for the rotation of an off center vortex around the trap center [28, 29]. In addition to this,

each vortex creates a velocity field varying inversely with the distance from its center, which is experienced by the other vortex of vortex dipole. If  $(x, y)$  and  $(x, -y)$  are the locations of the positively and negatively charged vortices of the vortex dipole, respectively, then the total velocity field experienced by the positively charged vortex of the vortex dipole

$$\mathbf{v}(x, y) = \omega_{\text{pr}} \hat{k} \times \mathbf{r} + \frac{1}{2y} \hat{i}, \quad (7)$$

where  $\omega_{\text{pr}}$  is the rotational frequency of a vortex with charge +1 in the condensate. In terms of component velocities, the previous equation can be written as

$$\begin{aligned} \frac{dx}{dt} &= -\omega_{\text{pr}} y + \frac{1}{2y}, \\ \frac{dy}{dt} &= \omega_{\text{pr}} x. \end{aligned} \quad (8)$$

This coupled set of differential equations describes the trajectory of the positively charged vortex of the vortex dipole. In the present work, we move the obstacle along  $x$ -axis, leading to the generation of vortex dipole located symmetrically about  $x$ -axis. Since  $y$  is small (and positive) for the positively charged vortex of the vortex dipole at the instant of generation, one can neglect  $-\omega_{\text{pr}} y$  in first equation of coupled Eqs.8 to obtain

$$\begin{aligned} \frac{dx}{dt} &\approx \frac{1}{2y}, \\ \frac{dy}{dt} &= \omega_{\text{pr}} x. \end{aligned} \quad (9)$$

Eqs.9 imply that vortex initially to the left of the origin moves towards origin with increasing speed along positive  $x$ -axis but decreasing speed along negative  $y$ -axis. At  $x = 0$ ,  $dy/dt = 0$  and beyond this vortex moves away from origin with decreasing speed along  $x$ -axis but increasing speed along positive  $y$ -axis. Near the origin  $\omega_{\text{pr}} x \ll 1/2y$ , then the velocity of the vortex can be approximated as

$$\mathbf{v}(x, y) \approx \frac{1}{2y} \hat{i}. \quad (10)$$

In this case the velocity of the vortex is mainly induced one, and it moves with induced velocity towards positive  $x$  direction. On the other hand if  $y$  is too large, one can neglect  $1/2y$  term in Eq.8 to obtain

$$\mathbf{v}(x, y) \approx \omega_{\text{pr}} \hat{k} \times \mathbf{r}. \quad (11)$$

In this case, the velocity of the vortex is mainly due to the inhomogeneous nature of the condensate, resulting in the rotation with frequency  $\omega_{\text{pr}}$ . The transition between vortex induced velocity to inhomogeneity induced velocity occurs when  $dx/dt = 0$ , i.e., velocity along  $x$ -axis changes sign. From Eqs.8, it occurs at  $y = \sqrt{1/2\omega_{\text{pr}}}$ .

### III. OBSTACLE MODIFIED CONDENSATE DENSITY

In the phase separated domain of binary condensates, the species with lower repulsion energy forms a core and the other species forms a shell around it. For convenience, we identify the former and later as the first and second species, respectively. With this labelling, interaction energies  $u_{11} < u_{22}$  and for equal populations this implies  $a_{11} < a_{22}$ . There is large difference of the local coherence length  $\xi_i = 1/\sqrt{2n_i u_{ii}}$  when  $u_{11} \ll u_{22}$ . This results in different density modifications for the two species when an obstacle beam is applied. The dynamics is most sensitive to the coherence length difference while the obstacle is crossing the interface layer of the binary condensate.

To analyze the density perturbations in presence of the obstacle beam, let  $R_{\text{in}}$  be the radius of the inner species or the interface boundary. And, let  $R_{\text{out}}$  be the radial extent of the outer species. In the absence of the obstacle beam, the chemical potential of first species is  $\mu_1 = R_{\text{in}}^2/4 + u_{11}/(\pi R_{\text{in}}^2)$ . Here, the second term is correction arising from the presence of the second species. The chemical potential of the second species is  $R_{\text{out}}^2/2$ . Both of these are in scaled units. We consider the obstacle beam initially ( $t = 0$ ) located at  $(-R_{\text{out}}, 0)$  and traversing towards the center with velocity  $v_{\text{obs}}$ . As it moves, its intensity is ramped down at the rate  $\eta$ . The location of the beam at a later time is

$$x_0(t) = -R_{\text{out}} + v_{\text{obs}}t, \quad (12)$$

and intensity of the beam is

$$V_0(t) = V_0(0) - \eta t, \quad (13)$$

where  $V_0(0)$  is the initial intensity of the obstacle beam. At the starting point, the total potential  $V(R_{\text{out}}, 0, 0) > R_{\text{out}}^2/2$  and the density of the outer species  $|\psi_2|^2$  is zero around the center of the obstacle beam as is shown in Fig. 1(a). However, as it traverses the condensates with de-

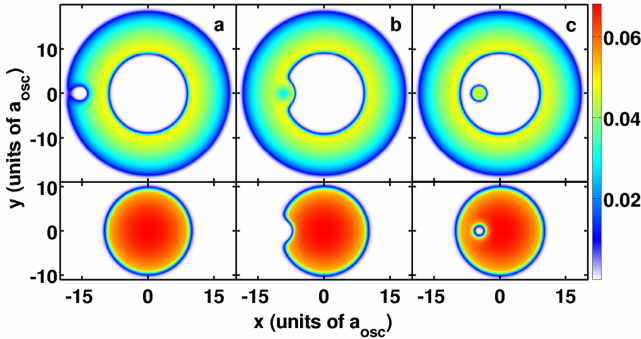


FIG. 1. The stationary state wave functions of  $^{85}\text{Rb}$ - $^{87}\text{Rb}$  binary condensate obtained from imaginary time propagation. For (a) the obstacle is located near  $R_{\text{out}}$ , for (b) the obstacle is located at the interface, and for (c) it is well inside the bulk of the inner species.

creasing intensity, at some later time  $t'$ ,  $V(x_0(t'), 0, 0) <$

$R_{\text{out}}^2/2$ . Density  $|\psi_2|^2$  is then finite within the obstacle. For compact notations, hereafter we drop the explicit notation of time dependence while writing  $x_0(t)$  and  $V_0(t)$ .

#### A. Density modification at interface

As the obstacle beam approaches the interface, the intensity is weak to expel out the outer species. However, when the beam enters the inner species with any finite intensity  $V(R_{\text{in}}, 0, t) > \mu_1$ , it is sufficient to make  $|\psi_1|^2$  zero around the beam [see Fig. 1(a)]. The interface is modified and equipotential curve of the interface is

$$\frac{x^2 + y^2}{2} + V_0 \exp \left[ -2 \frac{(x - x_0)^2 + y^2}{w^2} \right] = \frac{R_{\text{in}}^2}{2}. \quad (14)$$

Around the center of the obstacle beam,  $\sqrt{(x - x_0)^2 + y^2} < w/\sqrt{2}$ , and the obstacle potential is

$$V_{\text{opt}} \approx V_0 - \frac{2V_0}{w^2} [(x - x_0)^2 + y^2]. \quad (15)$$

Hence from Eq.(14) the equipotential curve in the neighborhood of the obstacle beam is

$$\left( x + \frac{C}{2A} \right)^2 + y^2 = \tilde{R}_{\text{in}}^2, \quad (16)$$

where

$$\begin{aligned} A &= \frac{1}{2} - \frac{2V_0}{w^2}, \\ C &= \frac{4V_0 x_0}{w^2}, \\ \tilde{R}_{\text{in}}^2 &= \frac{1}{A} \left( \frac{R_{\text{in}}^2}{2} + \frac{C^2}{4A} + C \frac{x_0}{2} - V_0 \right). \end{aligned}$$

Equipotential curve in the vicinity of the obstacle is thus modified into a circle with center at  $(-C/2A, 0)$  and radius  $\tilde{R}_{\text{in}}$ . In our numerical calculations, the Gaussian obstacle potential is quite narrow and  $w^2/(4V_0) \ll 1$ . Retaining only the leading order terms in  $w^2/4V_0$ , the center is approximately located at  $(x_0 + w^2 x_0/(4V_0), 0)$  and radius is

$$\tilde{R}_{\text{in}} \approx \sqrt{\frac{w^2}{2V_0} \left( 1 + \frac{w^2}{4V_0} \right) \left( V_0 + \frac{x_0^2}{2} - \frac{R_{\text{in}}^2}{2} \right)}. \quad (17)$$

Sufficiently away from the obstacle  $\sqrt{(x - x_0)^2 + y^2} > w/\sqrt{2}$  and the obstacle potential is negligible. The equipotential curve then remains unchanged,  $R_{\text{in}}^2 = x^2 + y^2$ . Thus an approximate piecewise expression of the equipotential curve is

$$\begin{aligned} \left( x + \frac{C}{2A} \right)^2 + y^2 &= \tilde{R}_{\text{in}}^2, \text{ if } |R_{\text{in}} - x_0| < \frac{w}{\sqrt{2}}, \\ x^2 + y^2 &= R_{\text{in}}^2, \text{ if } \sqrt{(x - x_0)^2 + y^2} > \frac{w}{\sqrt{2}}. \end{aligned}$$

This curve defines the interface geometry of the inner species in the TF approximation. Surface effects, however, smoothen the density profile around the meeting point of the two regions as is shown in Fig. 1(b). The obstacle beam is repulsive and expels the condensate around it such that bulk density is regained over a distance of one healing length.

### B. Fully immersed obstacle beam

A critical requirement to form coreless vortices is complete immersion of the obstacle beam within  $n_1$ . Based on the previous discussions, as the beam approaches the origin, the last point of contact between the beam and interface at  $R_{\text{in}}$  lies along  $x$ -axis. To determine the condition when complete immersion occurs, consider the total potential along  $x$ -axis

$$V(x, 0, t) \approx \frac{x^2}{2} + V_0(t) \left[ 1 - 2 \frac{(x - x_0(t))^2}{w^2} + 4 \frac{(x - x_0(t))^4}{w^4} \right], \quad (18)$$

where, the Gaussian beam potential is considered upto the second order term. The expression is appropriate in the neighborhood of the beam and has one local minima and maxima each. There is also a global minima, however, it is not the correct solution as it lies in the domain where  $x > \frac{w}{\sqrt{2}}$ . Correct global minima is the one located at  $x = 0$  and associated with the harmonic potential. The obstacle is considered well immersed when the local minima is located at the interfacial radius  $R_{\text{in}}$ . The local minima is a root of the polynomial

$$x^3 + a_2 x^2 + a_1 x + a_0 = 0, \quad (19)$$

obtained from the condition  $dV/dx = 0$ . Here,

$$\begin{aligned} a_2 &= -3x_0, \\ a_1 &= -\frac{w^2}{2} + 3x_0^2 + \frac{w^4}{8V_0}, \\ a_0 &= \frac{1}{2}x_0(w^2 - 2x_0^2). \end{aligned}$$

For the trapping potential parameters considered in the present work, all the three roots are real. The root corresponding to local minima is

$$x_{\text{min}}(t) = -\frac{(s_+ + s_-)}{2} - \frac{a_2}{3} + i\frac{\sqrt{3}}{2}(s_+ - s_-), \quad (20)$$

where

$$s_{\pm} = \left[ -\frac{a_2^3}{27} + \frac{1}{6}(-3a_0 + a_1 a_2) \pm \sqrt{\left(\frac{a_1}{3} - \frac{a_2^2}{9}\right)^3 + \left(-\frac{a_2^3}{27} + \frac{1}{6}(-3a_0 + a_1 a_2)\right)^2} \right]^{1/3}.$$

and  $x_{\text{min}}$  is a function of time as the obstacle potential is time dependent. However, for compact notations, like in  $V_0$  and  $x_0$ , hereafter we drop the explicit notation of time dependence while writing  $x_{\text{min}}(t)$ . Value of  $x_{\text{min}}$  is real when it satisfies certain conditions [30] and these are met for the experimentally realizable parameters. The obstacle is then completely immersed when  $x_{\text{min}} = R_{\text{in}}$  and let  $t_{\text{im}}$  denote the time at which this condition is satisfied. Once the obstacle beam is well inside the inner species, within the beam  $n_1$  is zero but  $n_2$  is nonzero. It then forms a second interface layer, assisted by the obstacle beam, which embeds a bubble of the  $n_2$  within  $n_1$ . Recollect, the first interface layer is located at  $R_{\text{in}}$  and it is where  $n_2$  encloses  $n_1$ . The second interface, unlike the one at  $R_{\text{in}}$ , is a deformed-ellipse and label it as  $\Gamma$ . It touches  $x$ -axis at two points and  $x_{\text{min}}$  is the one farther from the origin. From TF-approximation, the density of  $n_2$  within  $\Gamma$  is

$$n_{2\Gamma}(x, y, t_{\text{im}}) = \frac{\mu_2 - V(x, y, t_{\text{im}})}{u_{22}}, \quad (21)$$

where the subscript  $\Gamma$  is to indicate the density is within  $\Gamma$ . At  $t_{\text{im}}$ ,  $n_{2\Gamma}$  is in equilibrium with the bulk of  $n_2$ , and let the number of atoms in the be  $N_{2\Gamma}$ , which can be calculated from  $n_{2\Gamma}$ .

Except for deviations arising from mean field energy, the second interface  $\Gamma$  closely follows an equipotential surface. From the conditions of pressure balance at two interfaces

$$\begin{aligned} \mu_1 - \sqrt{\frac{u_{11}}{u_{22}}} \mu_2 &= \frac{R_{\text{in}}^2}{2} \left( 1 - \sqrt{\frac{u_{11}}{u_{22}}} \right), \\ \mu_1 - \sqrt{\frac{u_{11}}{u_{22}}} \mu_2 &= V(x_{\text{min}}, 0, t) \left( 1 - \sqrt{\frac{u_{11}}{u_{22}}} \right). \end{aligned} \quad (22)$$

The first equation is valid all along the interface at  $R_{\text{in}}$ . However, the second is derived at  $(r_{\text{min}}, 0)$ , but to a good approximation the condition is valid along  $\Gamma$  as it is close to an equipotential surface. The density of the first species at  $(x_{\text{min}}, 0)$  is

$$n_1(x_{\text{min}}) = \frac{1}{\sqrt{u_{11}u_{22}}} \left[ \frac{R_{\text{out}}^2 - 2V(x_{\text{min}}, 0, t)}{2} \right]. \quad (23)$$

Similarly density of second species at  $(x_{\text{min}}, 0)$  is

$$n_2(x_{\text{min}}) = \frac{1}{u_{22}} \left[ \frac{R_{\text{out}}^2 - 2V(x_{\text{min}}, 0, t)}{2} \right]. \quad (24)$$

Inside  $\Gamma$ , where the obstacle potential is dominant,  $n_1$  decays exponentially. Along the  $x$ -axis

$$n_1(\delta x_-, 0) = n_1(x_{\text{min}}, 0) \exp\left(-\frac{2}{\Lambda_1} \delta x_-\right), \quad (25)$$

where,  $\delta x_-$  is the distance of the point measured from  $\Gamma$ . Similarly the density of the second species just outside  $\Gamma$  is

$$n_2(\delta x_+, 0) = n_2(x_{\text{min}}, 0) \exp\left(-\frac{2}{\Lambda_2} \delta x_+\right), \quad (26)$$

where  $\delta x_+$  is distance from  $\Gamma$  but away from the obstacle beam, and  $\Lambda_2$  is the penetration depth of the second species. In these expressions the penetration depth is

$$\Lambda_i = \xi_i \left[ \frac{\sqrt{a_{11}a_{22}}}{a_{12} - \sqrt{a_{11}a_{22}}} \right]^{1/2}. \quad (27)$$

Based on the densities at the interface region, we can incorporate the interspecies interaction and calculate the effective potential of each species.

### C. Obstacle assisted bubble

At a time  $\Delta t$  after the obstacle is immersed in  $n_1$ , the location and amplitude of the obstacle potential are

$$x_0(t_{\text{im}} + \Delta t) = -R_{\text{out}} + v_{\text{ob}}(t_{\text{im}} + \Delta t), \quad (28)$$

$$V_0(t_{\text{im}} + \Delta t) = V_0(0) + v_{\text{ob}}(t_{\text{im}} + \Delta t). \quad (29)$$

Equilibrium TF  $n_2$  within the obstacle potential at this instant of time is

$$n_{2\Gamma}(x, y, t_{\text{im}} + \Delta t) = \frac{\mu_2 - V(x, y, t_{\text{im}} + \Delta t)}{u_{22}}. \quad (30)$$

This, however, is higher than the density distribution at  $t_{\text{im}}$ , that is  $n_{2\Gamma}(x, y, t_{\text{im}} + \Delta t) > n_{2\Gamma}(x, y, t_{\text{im}})$  as the potential  $V$  is lower. This is on account of two factors: first, the amplitude of the obstacle potential decreases with time; and second, the harmonic oscillator potential is lower at  $x_0(t_{\text{im}} + \Delta t)$ . The number of atoms, however, does not change from the value at  $t_{\text{im}}$  unless there is a strong Josephson current. Density  $n_{2\Gamma}$  is thus below the equilibrium value once the obstacle beam is well within  $n_1$ . This creates a stable bubble of  $n_2$  assisted or trapped within the beam and is transported through the  $n_1$ .

Departure of  $n_2$  from the equilibrium is not the only density evolution within the beam. There is a progressive change of  $n_{1\Gamma}$  as the beam moves deeper into  $n_1$ . At time  $t_{\text{im}}$ , when the obstacle is completely immersed in  $n_1$  the effective potential, experienced by  $n_1$ ,  $V(x, y, t_{\text{im}}) + n_{2\Gamma}u_{12}$  is larger than  $\mu_1$ . So,  $n_1$  is zero within the beam. However, if the rate of ramping  $\eta$  is such that at a later time  $V(x, y, t_{\text{im}} + \Delta t) + n_{2\Gamma}u_{12} < \mu_1$ , while the beam is still within  $n_1$ , there is a finite  $n_1$  within the beam.

$$n_{1\Gamma} = \frac{\mu_1 - V(x, y, t_{\text{im}} + \Delta t) - u_{12}n_{2\Gamma}}{u_{11}} \quad (31)$$

As the growth of  $n_{1\Gamma}$  is in its nascent stage, Eq. (30) is still applicable. Since  $a_{12} > \sqrt{a_{11}a_{22}}$  for the condensate, in TF approximation both  $n_{1\Gamma}$  and  $n_{2\Gamma}$  can not be simultaneously non-zero. At the same time,  $n_{2\Gamma}$  is forbidden to migrate to the bulk  $n_2$  due to the  $n_1$  generated potential barrier in the region between interfaces  $\Gamma$  and  $R_{\text{in}}$ . To accommodate both  $n_1$  and  $n_2$  within the beam, the shape of interface  $\Gamma$  is transformed to increase  $n_{2\Gamma}$ . So that  $n_2$  is zero in certain regions within the beam where the condition  $V(x, y, t_{\text{im}} + \Delta t) + n_{2\Gamma}u_{12} < \mu_1$  is satisfied. This mechanism is responsible for obstacle assisted transport of  $n_2$  across  $n_1$ .

### D. Obstacle induced density instability

The harmonic potential increases once the obstacle crosses origin, but the obstacle potential continues to decrease. A fine balance is achieved if

$$\frac{dV_{\text{obs}}}{dx} = \frac{\partial V_{\text{obs}}}{\partial x} + \left( \frac{dx}{dt} \right)^{-1} \frac{\partial V_{\text{obs}}}{\partial t}, \quad (32)$$

the dynamical rate of change of obstacle potential, is same in magnitude and opposite to the rate of change of the harmonic potential  $dV_{\text{ho}}/dx$ . It is, however, difficult to satisfy this condition across the entire obstacle potential as the Gaussian beam has different profile than the oscillator trapping potential. But, the parameters may be tuned so that the condition is satisfied at the center of the beam, then

$$\frac{dV_{\text{ho}}}{dx} = \frac{\eta}{v_{\text{obs}}}. \quad (33)$$

In the present case  $\eta$  is a constant and the condition in Eq. (33) is satisfied only when the beam is at a specific point  $x_e$ , then

$$\left. \frac{dV_{\text{ho}}}{dx} \right|_{x_e} = \frac{\eta}{v_{\text{obs}}} \quad (34)$$

Before reaching  $x_e$ , the potential within the beam decreases, but increases after crossing it. At some point beyond  $x_e$ , the total potential experienced by  $n_2$  bubble can become greater than  $\mu_2$ , resulting in an unstable bubble.

## IV. STABILITY OF CORELESS VORTEX DIPOLE

To analyze the energetic stability of coreless vortex dipoles in phase-separated binary condensates, we adopt the following *ansatz* for the wave function of inner and outer species

$$\begin{aligned} \psi_1(x, y) &= a [i(x - v_1) + (y^2 - v_2^2)] \exp\left(-\frac{x^2 + y^2}{2}\right), \\ \psi_2(x, y) &= b(x^2 + y^2) \exp\left(-\frac{x^2 + y^2}{2}\right), \end{aligned} \quad (35)$$

where  $(v_1, \pm v_2)$  is the location of the vortex dipole. With this choice of *ansatz*, the vortex dipole in the inner species is a normal vortex dipole. For simplicity of analysis, consider the trapping potential is purely harmonic, i.e.

$$V(x, y) = \frac{x^2 + y^2}{2}. \quad (36)$$

Normalization yields the following constraints on  $a$  and  $b$

$$\begin{aligned} a &= \left[ \frac{4}{5\pi + 4\pi(v_1^2 - v_2^2 + v_2^4)} \right]^{1/2}, \\ b &= \sqrt{\frac{1}{2\pi}}, \end{aligned} \quad (37)$$

and reduces the number of unknowns to two  $v_1$  and  $v_2$ . The energy of the binary condensate using the *ansatz* in Eq. (35) is

$$E = \frac{N_2 b^2}{\pi} \left( 4 + \frac{3}{8} b^2 u_{22} \right) + \frac{N_1 a^2 \pi}{1024} \{ 32 [8(11 + 4v_1^2 - 4v_2^2 + 4v_2^4) + b^2 u_{12} (15 + 8v_1^2 - 12v_2^2 + 8v_2^4)] + a^2 u_{11} [177 - 304v_2^2 + 256v_1^4 + 416v_2^4 - 256v_2^6 + 256v_2^8 + 32v_1^2 (15 - 8v_2^2 + 16v_2^4)] \}. \quad (38)$$

In the same way, we can also determine the chemical potentials of the two species in terms of the same parameters. The stationary points of the energy function are the solutions of the coupled equations  $\partial E / \partial v_1 = 0$  and  $\partial E / \partial v_2 = 0$ . These equations are solvable analytically, but the solutions are lengthy and cumbersome. The solution of particular interest is the vortex dipole located along the  $y$ -axis ( $v_1 = 0$ ). This is consistent with the observation that, regardless of the orientation, from the symmetry the axis passing through vortex dipole can be considered as the  $y$ -axis. A rotation transformation is sufficient to achieve this. For the case considered, the energy extrema conditions simplify to equations

$$\begin{aligned} \frac{\partial E}{\partial v_1} &= \frac{\pi a N_1}{256} \left\{ 16 [8(11 - 4v_2^2 + 4v_2^4) + b^2 u_{12} (15 - 12v_2^2 + 8v_2^4)] \frac{\partial a}{\partial v_1} + a^2 u_{11} [177 - 304v_2^2 + 416v_2^4 - 256v_2^6 + 256v_2^8] \frac{\partial a}{\partial v_1} \right\}, \\ \frac{\partial E}{\partial v_2} &= \frac{\pi a N_1}{256} \left\{ 64 a v_2 [8(2v_2^2 - 1) + b^2 u_{12} (4v_2^2 - 3)] - 8a^3 u_{11} v_2 [19 - 52v_2^2 + 48v_2^4 - 64v_2^6 (4v_2^2 - 1)] + 16 [8(11 - 4v_2^2 + 4v_2^4) + b^2 u_{12} (15 - 12v_2^2 + 8v_2^4)] \frac{\partial a}{\partial v_2} + a^2 u_{11} [177 - 304v_2^2 + 416v_2^4 - 256v_2^6 + 256v_2^8] \frac{\partial a}{\partial v_2} \right\}. \quad (39) \end{aligned}$$

For the sake of illustration, consider,  $N_1 = 10^5$ ,  $N_2 = N_1/2$ ,  $a_{11} = 0.99a_0$ ,  $a_{22} = 4.6a_0$ ,  $a_{12} = 2.14a_0$ ,  $\beta = 11.25$ ,  $\omega/2\pi = 8$ , and  $V_0(t) = 0$ . Call this set of parameters as parameters *set b*. The stationary points corresponding to minimum energy for this parameters set are  $(v_1, v_2) = (0, \pm 0.9678)$ .

### A. Coreless vortex dipole

To compare the energy of this normal vortex dipole with that coreless vortex dipole, consider that the cores of the vortices at  $(v_1, v_2)$  and  $(v_1, -v_2)$  are filled with outer species. We approximate the cores as circular with a radius of  $\xi = 1/\sqrt{2\mu_1}$ , the coherence length of the inner

species. We approximate the density profiles of the outer species within the cores with the TF distribution

$$\psi_2(x, y) = \begin{cases} \sqrt{\frac{\mu_2 - V(x, y)}{u_{22}}} & r_c^2 \leq \xi^2 \\ b(x^2 + y^2) \exp\left(-\frac{x^2 + y^2}{2}\right) & r_c^2 > \xi^2, \end{cases} \quad (40)$$

where  $r_c = \sqrt{(x - v_1)^2 + (y \pm v_2)^2}$  is the radial distance from the core of each vortex and antivortex. The above expression for  $\psi_2$  is renormalized to obtain the modified value of  $b$ , which in turn enables us to calculate the energy for the coreless vortex dipole. To obtain the analytic expression for energy, we integrate  $b(x^2 + y^2) \exp\left(-\frac{x^2 + y^2}{2}\right)$  over the whole real space without excluding the core regions. The modified value of  $b$  after the normalization is

$$b \approx \left[ \frac{2u_{22} - \pi\xi^2 (\xi^2 + 2v_1^2 + 2v_2^2 - 4\mu_2)}{4\pi u_{22}} \right]^{1/2}. \quad (41)$$

With this approximation, the number of atoms of outer species embedded within the cores is

$$\delta N_2 = N_2 \frac{\pi\xi^2 (\xi^2 + 2v_1^2 + 2v_2^2 - 4\mu_2)}{2u_{22}}. \quad (42)$$

These contribute to the total energy through the potential and intra-species interaction energies. The energy contribution from the cores is then

$$\delta E = -\frac{\pi\xi^2}{12u_{22}} [\xi^4 + 3v_1^4 + 6\xi^2 v_2^2 + 3v_2^4 + 6v_1^2 (\xi^2 + v_2^2) - 12\mu_2^2]. \quad (43)$$

The total energy of the binary condensate with coreless vortex is

$$E_c = E + \delta E, \quad (44)$$

where  $E$  is defined by Eqs. (38) and (41). For the parameter *set b*, the energy per particle  $[E_c/(N_1 + N_2)]$  is 4.18 which is smaller than the value of 4.26 obtained from Eqs. (37) and (38). This implies that coreless vortex dipole is energetically more favorable than normal vortex dipole with the percentage energy difference of 1.9%.

The Gaussian form of the *ansatz* imposes limitations on the domain of applicability. But, the *ansatz* provide qualitative information on the stability coreless vortex dipoles. To relate to experimental realizations, consider  $^{85}\text{Rb}$ - $^{87}\text{Rb}$  binary condensate with  $a_{11} = 460a_0$ ,  $a_{22} = 99a_0$ , and  $a_{12} = 214a_0$  as the scattering length values and  $2N_1 = N_2 = 10^6$  as the number of atoms. Here  $a_{11}$  is tunable with magnetic Feshbach resonance [31]. With this set of parameters, the stationary state of  $^{85}\text{Rb}$ - $^{87}\text{Rb}$  binary condensate is just phase-separated. The trapping potential and obstacle laser potential parameters are same as those considered in Ref.[6], that

is  $\omega/(2\pi) = 8\text{Hz}$ ,  $\alpha = 1$ ,  $\beta = 11.25$ ,  $V_0(0) = 93.0\hbar\omega$ , and  $w_0 = 10\mu\text{m}$ . Hereafter we term this set of scattering lengths, number of atoms, and trapping potentials as *set a*. For this parameter set, in absence of the obstacle potential, the stationary point of minimum energy is  $(v_1, v_2) = (0, \pm 0.75275)$ . And, the difference in the energies per particle of the binary condensate with normal and coreless vortex dipoles is 0.11.

### B. TF approximation single vortex

As mentioned earlier, the applicability of the variational *ansatz* is limited to the weakly interacting domain. Experiments, however, mostly explore domains other than weakly interacting. To analyze stability in this domain, we resort to the TF approximation.

#### 1. Normal vortex

To simplify the analysis, consider a normal vortex located at the center of the inner species. For a normal vortex, the wave functions of the first or inner species in TF approximation is

$$\psi_1(r) = \begin{cases} \sqrt{\frac{\mu_1 - V(r)}{u_{11}}} \frac{r}{\sqrt{r^2 + \xi^2}} & r^2 \leq R_{\text{in}}^2, \\ 0 & r^2 > R_{\text{in}}^2. \end{cases} \quad (45)$$

Similarly, the wave function of the second or outer species is

$$\psi_2(r) = \begin{cases} \sqrt{\frac{\mu_2 - V(r)}{u_{22}}} & R_{\text{in}}^2 \leq r^2 \leq R_{\text{out}}^2 \\ 0 & r^2 > R_{\text{out}}^2 \end{cases} \quad (46)$$

here  $V(r)$ ,  $R_{\text{in}}$ ,  $R_{\text{out}}$ , and  $\xi$  are the trapping potential, radius of the interface between inner and outer species, radial extent of outer species, and coherence length of inner species, respectively. The chemical potentials  $\mu_1$  and  $\mu_2$  are parameters of the calculations and obtained from inverting the normalization condition

$$N_1 = \frac{\pi}{8u_{11}\mu_1^2} [2R_{\text{in}}^2 (\mu_1 + 4\mu_1^3) - 2R_{\text{in}}^4 \mu_1^2 + \ln(1 + 2R_{\text{in}}^2 \mu_1) \times (1 + 4\mu_1^2)] \quad (47)$$

$$N_2 = \frac{\pi (R_{\text{in}}^2 - 2\mu_2)^2}{4u_{22}}. \quad (48)$$

The total energy of the vortex with a normal vortex located at origin is

$$E = \int \left\{ \psi_1(r) \left[ -\frac{1}{r} \frac{\partial}{\partial r} - \frac{\partial^2}{\partial r^2} + \frac{1}{r^2} + V(r) + \frac{u_{11}}{2} |\psi_1(r)|^2 \right] \right. \\ \left. \psi_1(r) + \psi_2(r) \left[ V(r) + \frac{u_{22}}{2} |\psi_2(r)|^2 \right] \psi_2(r) \right\}, \quad (49)$$

The energy can be minimized under the constraint that  $\mu_1$  and  $\mu_2$  satisfy Eqs. (47-48) to completely determine the stationary state of binary condensate with a normal vortex at the origin.

#### 2. Coreless Vortex

For a coreless vortex, the wave functions of the two species in TF approximation are

$$\psi_1(r) = \begin{cases} \sqrt{\frac{\mu_1 - V(r)}{u_{11}}} \frac{r}{\sqrt{r^2 + \xi^2}} & r^2 \leq R_{\text{in}}^2 \\ 0 & r^2 > R_{\text{in}}^2, \end{cases} \quad (50)$$

$$\psi_2(r) = \begin{cases} \sqrt{\frac{\mu_2 - V(r) - u_{12}\psi_1(r)^2}{u_{22}}} & r^2 \leq \xi^2 \\ \sqrt{\frac{\mu_2 - V(r)}{u_{22}}} & R_{\text{in}}^2 \leq r^2 \leq R_{\text{out}}^2 \\ 0 & r^2 > R_{\text{out}}^2. \end{cases} \quad (51)$$

Normalizing the wave functions gives the constraint equations in terms of  $\mu_1$  and  $\mu_2$  as

$$N_1 = \frac{\pi}{8u_{11}\mu_1^2} [2R_{\text{in}}^2 (\mu_1 + 4\mu_1^3) - 2R_{\text{in}}^4 \mu_1^2 + \ln(1 + 2R_{\text{in}}^2 \mu_1) \times (1 + 4\mu_1^2)],$$

$$N_2 = \frac{\pi}{16u_{11}u_{22}\mu_1^2} \{u_{21} [-1 + \ln 4 + 8(\ln 2 - 1)\mu_1^2] + u_{11} \times (4R_{\text{in}}^4 \mu_1^2 + 8\mu_1 \mu_2 - 16R_{\text{in}}^2 \mu_1^2 \mu_2 + 16\mu_1^2 \mu_2^2 - 1)\} \quad (52)$$

From the expressions, we can calculate the total energy of the system. It is a complicated expression which we refrain from writing. For the present case, it is perhaps sufficient to say, it is possible to obtain an analytical but cumbersome expression of total energy.

For the parameter *set a* with  $V_0(t) = 0$ , binary condensate with the coreless vortex has lower energy than the one with normal vortex. This is evident from Fig.2 where the variation of total energy is shown as a function of  $R_{\text{in}}$ . However, the stability vanishes if one considers  $N_1 = N_2 = 10^6$ ,  $a_{11} = 51a_0$ ,  $a_{22} = 99a_0$  in *set a*. It is then the normal vortex which is energetically stable. This is evident from Fig.3. These results are in very good agreement with numerical results. This TF analysis, albeit, is for single vortex clearly illustrates that depending upon the interaction parameters, a phase-separated binary condensate can either support coreless or normal vortex. It must be emphasized, the energy, chemical potentials, and interface radius obtained from the TF approximation are in very good agreement with numerical solution of coupled GP equations. For example, the numerical value of energy 66.32 corresponding to Fig.3 is very close to the value 66.06 from TF approximation.

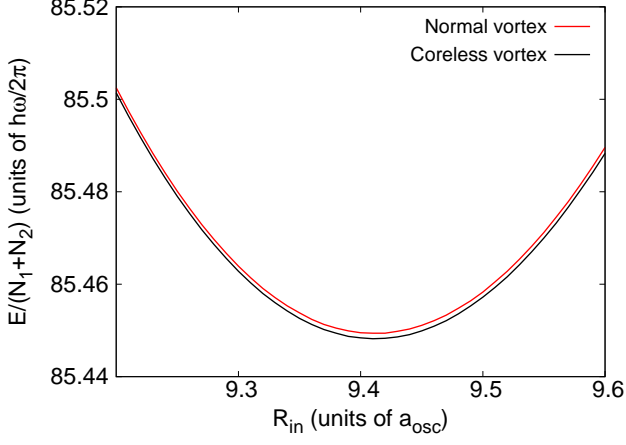


FIG. 2. The energy of the binary condensate with  $V_0 = 0$  and rest of the parameters same as those in the parameters *set a* as a function of  $R_{\text{in}}$ . The condensate has a vortex dipole located at origin. Black and blue curves are for coreless and normal vortex dipoles respectively.

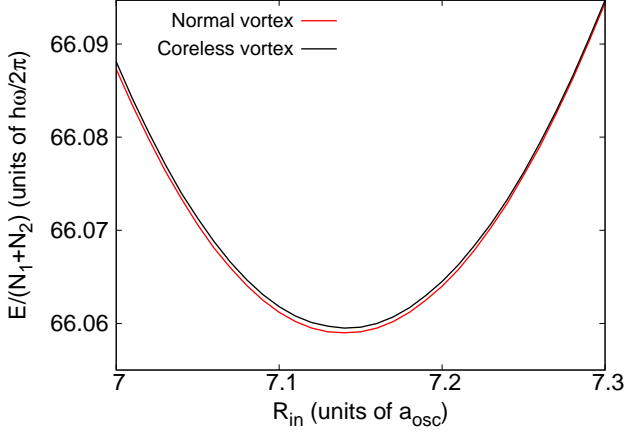


FIG. 3. The energy of the binary condensate with  $N_1 = N_2 = 10^6$ ,  $a_{11} = 51a_0$ ,  $a_{22} = 99a_0$ ,  $V_0 = 0$ , and rest of the parameters same as those in parameters *set a* as a function of  $R_{\text{in}}$ . The condensate has a vortex located at the origin. Black and blue curves are for coreless and normal vortex dipoles respectively.

### C. TF approximation with vortex dipole

We use the TF approximation to examine the stability of coreless vortices in the strongly interacting domain.

#### 1. Normal vortex dipole

Assume the vortex affects the density of the condensate only within the core regions. We then adopt the following *ansatz* for binary condensate with a normal vortex dipole

at  $(v_1, \pm v_2)$ .

$$\psi_1(r) = \begin{cases} 0 & x^2 + y^2 > R_{\text{in}}^2 \\ 0 & [(x - v_1)^2 + (y \pm v_2)^2] \leq \xi^2 \\ \sqrt{\frac{\mu_1 - V(x, y)}{u_{11}}} & \begin{cases} x^2 + y^2 \leq R_{\text{in}}^2 \text{ \& } \\ [(x - v_1)^2 + (y \pm v_2)^2] > \xi^2 \end{cases} \end{cases} \quad (53)$$

$$\psi_2(r) = \begin{cases} \sqrt{\frac{\mu_2 - V(x, y)}{u_{22}}} & R_{\text{in}}^2 \leq (x^2 + y^2) \leq R_{\text{out}}^2 \\ 0 & (x^2 + y^2) > R_{\text{out}}^2 \\ 0 & (x^2 + y^2) < R_{\text{in}}^2. \end{cases} \quad (54)$$

The vortex dipole contributes mainly through the kinetic energy of  $\psi_1$ , which may be approximated with the value of single species condensate given in Ref.[32]

$$E_{\text{vd}} = \frac{2\mu_1}{u_{11}} \ln \left( \frac{2v_2}{\xi} \right). \quad (55)$$

Using these *ansatz* the number of atoms are

$$N_1 = \frac{\pi (1 + 4v_1^2\mu_1 + 4v_2^2\mu_1 - 8\mu_1^2 - 2R_{\text{in}}^4\mu_1^2 + 8R_{\text{in}}^2\mu_1^3)}{8u_{11}\mu_1^2},$$

$$N_2 = \frac{\pi (R_{\text{in}}^2 - 2\mu_2)^2}{4u_{22}}. \quad (56)$$

In a similar way, we can evaluate the energy of the entire condensate.

#### 2. Coreless vortex dipole

For coreless vortex dipole, we adopt the *ansatz*

$$\psi_1(r) = \begin{cases} 0 & x^2 + y^2 > R_{\text{in}}^2 \\ 0 & [(x - v_1)^2 + (y \pm v_2)^2] \leq \xi^2 \\ \sqrt{\frac{\mu_1 - V(x, y)}{u_{11}}} & \begin{cases} x^2 + y^2 \leq R_{\text{in}}^2 \text{ \& } \\ [(x - v_1)^2 + (y \pm v_2)^2] > \xi^2, \end{cases} \end{cases} \quad (57)$$

$$\psi_2(r) = \begin{cases} \sqrt{\frac{\mu_2 - V(x, y)}{u_{22}}} & \begin{cases} R_{\text{in}}^2 \leq (x^2 + y^2) \leq R_{\text{out}}^2 \text{ \& } \\ [(x - v_1)^2 + (y \pm v_2)^2] \leq \xi^2 \end{cases} \\ 0 & (x^2 + y^2) > R_{\text{out}}^2 \\ 0 & \begin{cases} x^2 + y^2 < R_{\text{in}}^2 \text{ \& } \\ [(x - v_1)^2 + (y \pm v_2)^2] > \xi^2. \end{cases} \end{cases} \quad (58)$$

Using these *ansatz* the modified expressions for  $N_2$  is

$$N_2 = \frac{\pi}{8u_{22}\mu_1^2} (2R_{\text{in}}^4\mu_1^2 + 8\mu_1\mu_2 - 8R_{\text{in}}^2\mu_1^2\mu_2 + 8\mu_1^2\mu_2^2 - 1 - 4v_1^2\mu_1 - 4v_2^2\mu_1). \quad (59)$$

We can also calculate the total energy  $E$  of the system. The important change in  $E$  is the inclusion of interface



interaction energy  $E_{\text{int}}$ . It arises from the interface interactions at the cores of the vortex and antivortex. Based on Ref. [21],

$$E_{\text{int}} = \frac{8}{3} P b \pi \xi \left( \frac{a_{12}}{\sqrt{a_{11} a_{22}}} - 1 \right), \quad (60)$$

where  $P$  is the pressure on the circumference of the cores and

$$b = 2 \left[ \frac{3(\mu_1 + \mu_2) \sqrt{a_{11} a_{22}}}{4\mu_1 \mu_2 (a_{12} - \sqrt{a_{11} a_{22}})} \right]^{1/2}. \quad (61)$$

As in the previous section, energy can be minimized with the constraint of the fixed number of atoms. For the parameters *set a* without obstacle potential, the coreless vortex dipole has lower energy than the normal vortex dipole and is shown in Fig. 4 for the vortex dipole located at  $(0, \pm 1)$ .

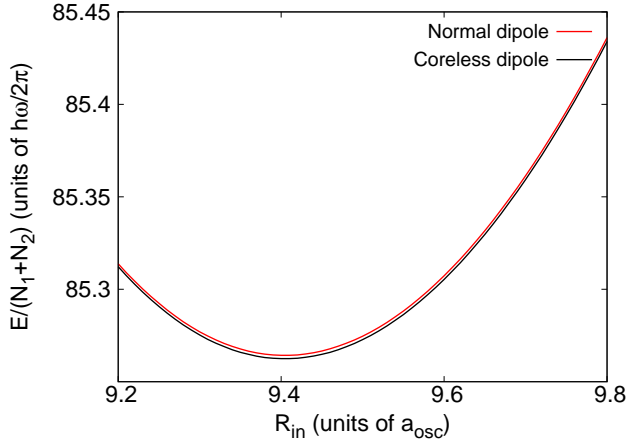


FIG. 4. The energy of the binary condensate with  $V_0 = 0$  and rest of the parameters same as those in the parameters *set a* as a function of  $R_{\text{in}}$ . The condensate has a vortex dipole located at  $(0, \pm 1)$ . Black and blue curves are for coreless and normal vortex dipoles respectively.

For  $N_1 = N_2 = 10^6$ ,  $a_{11} = 51a_0$ ,  $a_{22} = 99a_0$  and rest of the parameters same as in parameter *set a*, condensate with the normal vortex dipole has lower energy than the one with coreless vortex dipole (see Fig. 5). These results are again in good agreement with the numerical results.

## V. NUMERICAL RESULTS

For the numerical calculations, we again resort to experimentally realizable system and parameters. We again work with the  $^{85}\text{Rb}$ - $^{87}\text{Rb}$  mixture and parameter *set a* introduced earlier. Recall, the values of parameters in this set are  $a_{11} = 460a_0$ ,  $a_{22} = 99a_0$ , and  $a_{12} = 214a_0$ .  $2N_1 = N_2 = 10^6$ ,  $\omega/(2\pi) = 8\text{Hz}$ ,  $\alpha = 1$ ,  $\beta = 11.25$ ,

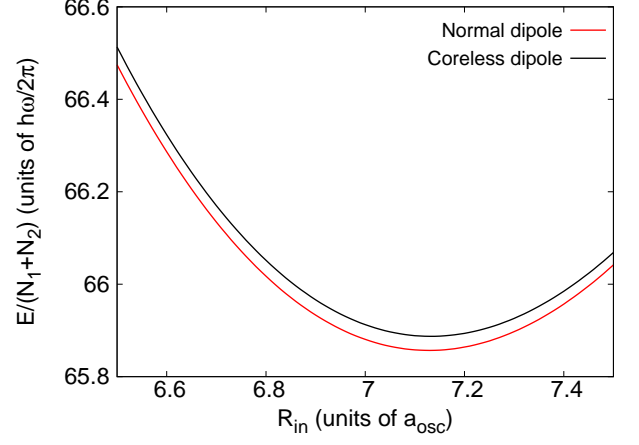


FIG. 5. The energy of the binary condensate with  $N_1 = N_2 = 10^6$ ,  $a_{11} = 51a_0$ ,  $a_{22} = 99a_0$ ,  $V_0 = 0$ , and rest of the parameters same as those in parameters *set a* as a function of  $R_{\text{in}}$ . The condensate has vortex dipole located at  $(0, \pm 1)$ . Black and blue curves are for coreless and normal vortex dipoles respectively.

$V_0(0) = 93.0\hbar\omega$ , and  $w_0 = 10\mu\text{m}$ . As mentioned earlier,  $a_{11}$  is tunable with magnetic Feshback resonance [31].

The transport of  $n_2$  within the region of influence of  $V_{\text{obs}}$  is crucial to generate coreless vortices. As  $V_{\text{obs}}$  enters  $n_1$ , it nudges  $n_1$  and creates an interstice, which is occupied by  $n_2$ . This is an outcome of the difference in coherence lengths ( $\xi_i = 1/\sqrt{2n_i u_{ii}}$ ). The smaller  $\xi$  of  $n_2$  ensures that it recovers bulk value over shorter distances. It implies that it is comparatively more difficult to displace the  $n_2$  than  $n_1$ . As the obstacle reaches the interface with diminished strength, it is unable to displace  $n_2$ , but not for  $n_1$  due larger  $\xi$ . This results in an inward protrusion of the interface, which detaches from the interface at a later time. For detachment to occur, it should be energetically favorable. The difference in  $\xi$  coupled with  $a_{12} \gtrsim \sqrt{a_1 a_2}$  ensures that the interstitial filling of  $n_2$  is energetically lower, in other words energetically favorable. This is easily confirmed with imaginary time propagation of GP equation to obtain the stationary state geometry of the binary condensate with  $V_{\text{obs}}$  located inside  $n_1$  as is shown in Fig. 1(c).

### A. Motion of $V_{\text{obs}}$ towards interface

We first consider the motion of  $V_{\text{obs}}$ , initially located in the  $n_2$  towards the interface. For this case, we consider  $^{85}\text{Rb}$ - $^{87}\text{Rb}$  binary condensate with parameter *set a* and  $V_{\text{obs}}$  of  $V_0(0) = 125.0$ . The  $V_{\text{obs}}$  is initially located at  $x = -15a_{\text{osc}}$  and moves with the speed of  $180\mu\text{m/s}$ . It progressively decreases in strength and vanishes at  $x = 8a_{\text{osc}}$ . The obstacle creates a normal vortex dipole as it traverses  $n_2$ . And, as  $V_{\text{obs}}$  approaches the interface, it transports the vortex dipole. Further motion of  $V_{\text{obs}}$  in the  $n_1$  generates coreless vortices in the inner com-

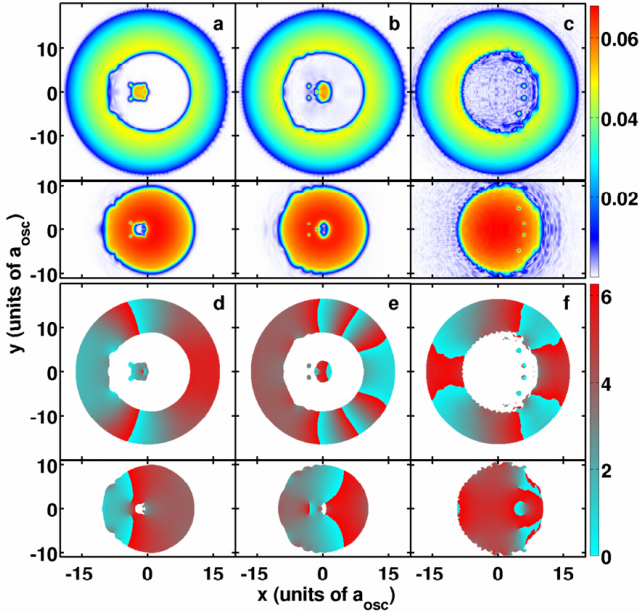


FIG. 6. Coreless vortex dipole shedding when the obstacle potential traverses from the edge to the inner component in a binary condensate with  $V_0 = 125$ ,  $x_0(0) = -15a_{\text{osc}}$  and rest of the parameters same as those in *set a*. Figures a, b and c are the absolute values of wave functions at 0.21s, 0.33s, 0.56s, respectively; while figures d, e and f are the corresponding phase plots.

ponent. The formation of the coreless vortex dipole is shown in Fig. 6. The plots in the figure show both the density and phase distribution. From the phase plot, it is clear that the phase singularity of the vortex is associated with  $n_1$ . And, from the density plot it is evident that the vortex-antivortex cores are filled with  $n_2$ . One effect which precedes the seeding of coreless vortex is the indentation of the inner interface after it cleaves when the  $V_{\text{obs}}$  is fully immersed in  $n_1$ . This may be explained in terms of the dynamical evolution around  $V_{\text{obs}}$  and analyzed in two different ways.

### 1. Inertia of $n_2$

Just after the interface cleaves, when the  $V_{\text{obs}}$  is set into motion at  $t = t_0$ , the  $n_2$  due to inertia, does not follow  $V_{\text{obs}}$  initially. As a result at  $t_0 + \delta t$ , neglecting the back flow of  $n_2$ , outer species (along  $x$ -axis) at  $x' \in [x_{\min}(t_0), x_{\min}(t_0 + \delta t)]$  is approximately same

$$n_2(x', 0, t + \delta t) \approx n_2(x', 0, t_0), \quad (62)$$

here  $\delta t$  is time taken by the outer species to redistribute itself according to the displaced obstacle potential. As a result over a length  $x_{\min}(t_0 + \delta t) - x_{\min}(t_0)$ , the density of inner species in TF approximation is

$$n_1(x', 0, t_0 + \delta t) = \frac{\mu_1 - x'^2/2 - n_2(x', t_0)u_{12}}{u_{11}}. \quad (63)$$

Hence inner  $n_1$  flows into the above domain and replaces  $n_2$ . The circular symmetry of  $V_{\text{obs}}$  coupled with motion along  $x$ -axis ensures that the aforementioned process starts along  $x$ -axis earlier; also the replacement of  $n_2$  by  $n_1$  takes place at the much faster speed as compared to the speed of the obstacle. This leads to creation of dimple on the inner interface.

### 2. Pressure balance

Let  $x_0$  and  $\Gamma_{x_0}$  be the location of the obstacle just after the interface cleaves and approximately circular inner interface centered around  $x_0$  with radius  $\tilde{R}_{\text{in}}$ , respectively. After time  $\delta t$ , let  $x'_0 = x_0 + \delta x_0$  and  $\Gamma_{x'_0}$  be the location of the obstacle and inner interface, respectively. Assuming that  $\Gamma_{x'_0}$  has same radius as  $\Gamma_{x_0}$ , i.e.  $\tilde{R}_{\text{in}}$ , the points of intersection of  $\Gamma_{x_0}$  and  $\Gamma_{x'_0}$  are

$$(x_c, y_c) = \left( \frac{1}{2}(x_0 + x'_0), \pm \frac{1}{2}\sqrt{4\tilde{R}_{\text{in}}^2 - \delta x_0^2} \right). \quad (64)$$

Thus the region  $\delta\Gamma$  defined as

$$(x - x_0)^2 + y^2 < \tilde{R}_{\text{in}}^2 < (x - x'_0)^2 + y^2 \quad (65)$$

with area

$$A = \pi\tilde{R}_{\text{in}}^2 - 2\tilde{R}_{\text{in}}^2 \cos^{-1} \frac{\delta x_0}{2\tilde{R}_{\text{in}}} + \frac{\delta x_0}{2} \sqrt{4\tilde{R}_{\text{in}}^2 - \delta x_0^2}, \quad (66)$$

lies within  $\Gamma_{x_0}$  but outside  $\Gamma_{x'_0}$ . Let  $P_1 = n_1^2 u_{11}/2$  and  $P_2 = n_2^2 u_{22}/2$  be the pressures exerted by inner and outer species on the left arc of  $\delta\Gamma$  region, respectively. The potential experienced by  $n_1$  along the left arc of  $\delta\Gamma$ , which is approximately equal to harmonic trapping potential, does not change as the obstacle is moving away from this region, and so does the  $P_1$ . The potential experienced by  $n_2$  over  $\delta\Gamma$ , which is equal to sum total of harmonic trapping and obstacle potentials, decreases as the obstacle moves from  $x_0$  to  $x_0 + \delta x_0$ . In fact, as one moves from  $(x', 0)$ , where  $x' \in (x_0 - \tilde{R}_{\text{in}}, x_0 + \delta x_0 - \tilde{R}_{\text{in}})$ , to the  $(x_c, y_c)$  along a curve with same sign of curvature as bounding arcs of  $\delta\Gamma$  region, the potential experienced by  $n_2$  decreases. This leads to the redistribution of  $n_2$ , i.e. it moves to the regions with weaker trapping potential. The redistribution will lead to  $\delta P = P_1 - P_2 > 0$  which decreases as one moves along the aforementioned curve. This will lead to indentation of the inner interface. In our simulations, when the obstacle is moved, along  $x$ -axis, from a point near the center towards the outer interface, indentation is suppressed. It confirms that this mechanism indeed aids the indentation of the interface.

### B. Obstacle motion towards edge

In this case, we start with the stationary state solution of  $^{85}\text{Rb}$ - $^{87}\text{Rb}$  binary condensate for the parameters *set*

$a$  with obstacle laser potential maxima located at  $x = -5.0a_{\text{osc}}$ . The static solution in this case is shown in first column of Fig.7, which has roughly doughnut shaped density distribution of the outer species along with non-zero density in the circle of influence of the obstacle.

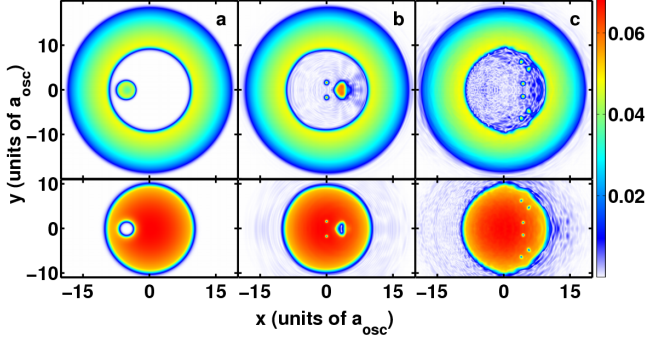


FIG. 7. The generation of triply charged vortex dipole in the  $^{85}\text{Rb}$ - $^{87}\text{Rb}$  binary condensate with parameters *set a*. The obstacle potential, initially located at  $x = -5.0a_{\text{osc}}$ , is moved with a velocity of  $220\mu\text{m/s}$  up to  $x = 5a_{\text{osc}}$ . First, second, and third columns are the solutions at  $t = 0\text{s}$ ,  $t = 0.14\text{s}$  and  $t = 0.32\text{s}$ , respectively.

Such density distributions are prerequisite to create coreless vortices in the inner species. The obstacle is moved with a uniform speed of  $220\mu\text{m/s}$ , progressively decreases in strength, and finally becomes zero at  $x = 5.0a_{\text{osc}}$ . With this velocity, we observe the creation of triply charged coreless vortex dipole as is shown in last column of Fig.7. Singly and doubly charged vortex dipoles can be generated by moving the obstacle potential at lower velocities. For example, Fig.8 shows the singly charged coreless vortex dipole and the trajectory followed by it for the  $^{85}\text{Rb}$ - $^{87}\text{Rb}$  binary condensate with parameters *set a*. The obstacle laser potential moves from  $x = 0a_{\text{osc}}$  at  $t = 0\text{s}$  to  $x = 8.0a_{\text{osc}}$  with the speed of  $200\mu\text{m/s}$ .

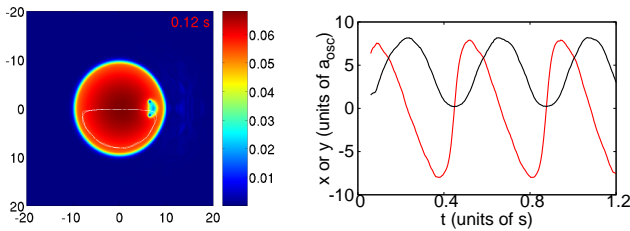


FIG. 8. The figure on the left side shows the vortex dipole in  $^{85}\text{Rb}$ - $^{87}\text{Rb}$  condensate with parameters *set a* at  $t = 0.12\text{s}$ . The white curve indicates the trajectory of lower vortex. The figure on the right side shows the variation in position of the upper vortex with time.

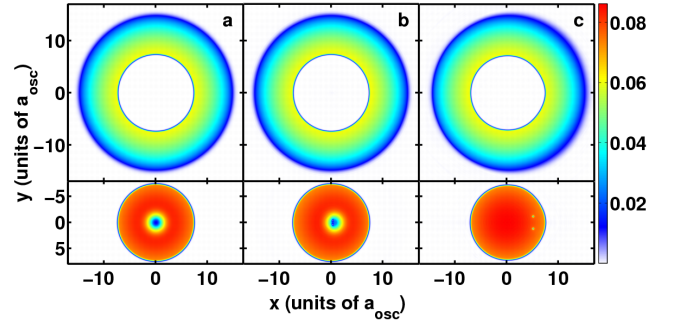


FIG. 9. The generation of normal vortex dipoles in the  $^{85}\text{Rb}$ - $^{87}\text{Rb}$  binary condensate with  $a_{11} = 51a_0$ ,  $N_1 = N_2 = 10^6$ , and the rest of the parameters same as those defined in parameters *set a*. The obstacle potential, initially located at  $x = 0a_{\text{osc}}$ , is moved with a velocity of  $200\mu\text{m/s}$  up to  $x = 5a_{\text{osc}}$ . First, second, and third columns are the absolute values of wave functions at  $t = 0\text{s}$ ,  $t = 0.01\text{s}$ , and  $t = 0.14\text{s}$ , respectively.

We also considered the  $^{85}\text{Rb}$ - $^{87}\text{Rb}$  with  $a_{11} = 51a_0$ ,  $N_1 = N_2 = 10^6$ , and the rest of the parameters same as those in parameter *set a*. The obstacle laser potential is initially located at origin  $x = 0a_{\text{osc}}$ . The stationary solution in this case is strongly phase separated ( $a_{12} \gg \sqrt{a_1 a_2}$ ), and the circular region of influence of obstacle potential is devoid of atoms of outer component as is shown in first column of Fig.9. In our simulation, the obstacle potential potential traverses a distance of  $5a_{\text{osc}}$  along x-axis with a speed of  $200\mu\text{m/s}$ . We observe that the vortex dipole generated in the inner component is a normal vortex dipole with empty core. This is consistent with the TF results shown in Fig. 5.

## VI. CONCLUSIONS

We have studied the motion of the Gaussian obstacle potential through a phase-separated binary condensate in pan-cake shaped traps. The motion of the obstacle leads to the generation of either coreless or normal vortex dipole depending upon the interaction parameters. The interaction parameters suitable for coreless vortex dipole can also be employed to have obstacle assisted transport of one species across another. We have used both a variational *ansatz* based method, applicable when  $N_i a_{ii}/a_{\text{osc}} \sim 1$ , and TF approximation based method, applicable when  $N_i a_{ii}/a_{\text{osc}} \gg 1$ , to analyze the energetic stability of coreless versus normal vortices. Our studies show that using Feshback resonances to tune one of the scattering length, e.g. scattering length of  $^{85}\text{Rb}$  in  $^{85}\text{Rb}$ - $^{87}\text{Rb}$ , it should be experimentally possible to create coreless vortices in phase-separated binary condensates.

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